

Optimizing antennas for phased array high frequency radars

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UH-UABC monopole (2008): 11.5 MHz



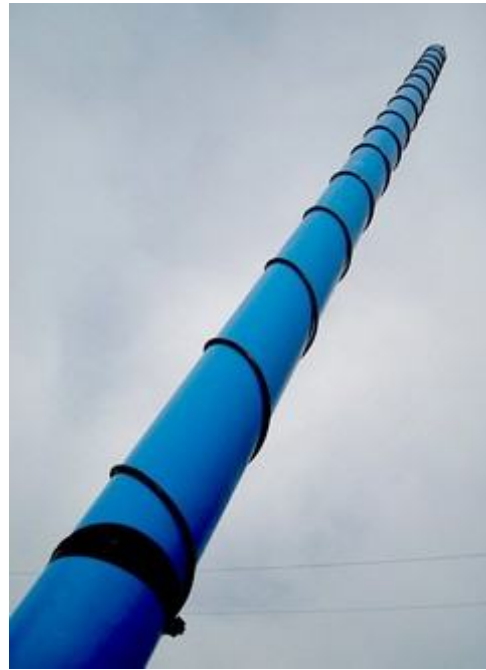
- $\lambda/4$ wire coiled on $\lambda/8$ bamboo
- geometric scaling defines frequency
- base coil-loading for tuning
- fully waterproof, potted junctions, RG213 pig-tail
- 4 buried $\lambda/4$ wire radials, approximate impedance 50Ω VSWR 1.1-1.2
- wide band $>f/30$

UH-UABC monopole (2008): 8 MHz



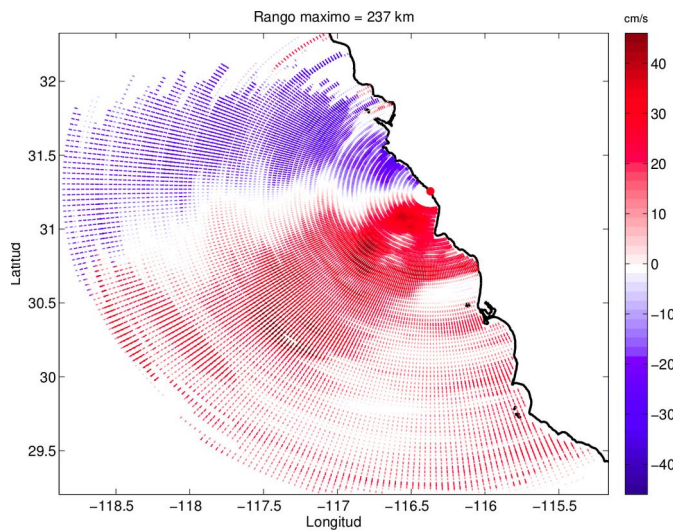
- $\lambda/4$ wire coiled on $\lambda/8$ fiberglass
- geometric scaling defines frequency
- base coil-loading for tuning
- fully waterproof, potted junctions, RG213 pig-tail
- 4 buried $\lambda/4$ wire radials, approximate impedance 50Ω VSWR 1.1-1.2
- wide band $f/30$

UH-UABC monopole (2008): 16 MHz



- $\lambda/4$ wire coiled on $\lambda/8$ PVC pipe
- geometric scaling defines frequency
- base coil-loading for tuning
- fully waterproof, potted junctions, RG213 pig-tail
- 4 buried $\lambda/4$ wire radials, approximate impedance 50Ω VSWR 1.1-1.2
- wide band $f/30$

UH-UABC monopole (2008): 8 MHz

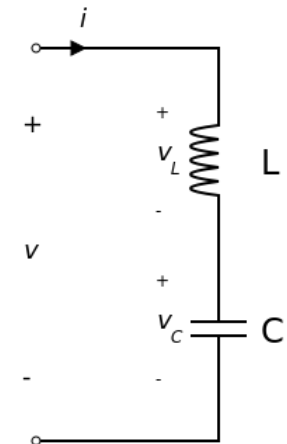


- $\lambda/4$ wire coiled on $\lambda/8$ treated wood
- geometric scaling defines frequency
- base coil-loading for tuning
- fully waterproof, potted junctions, RG213 pig-tail
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UH-UABC monopole (2008): 16 MHz



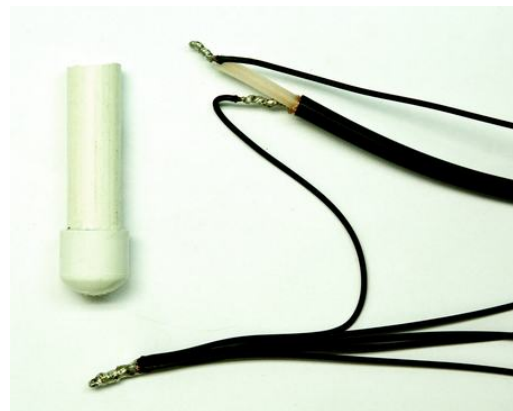
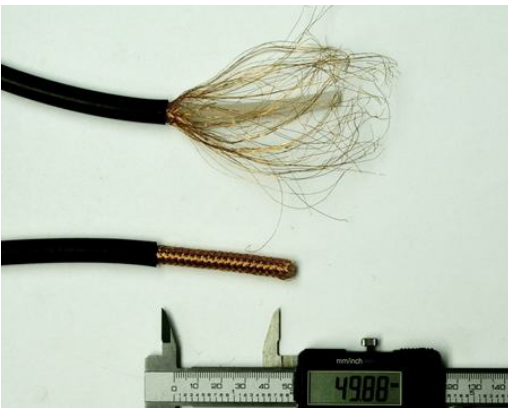
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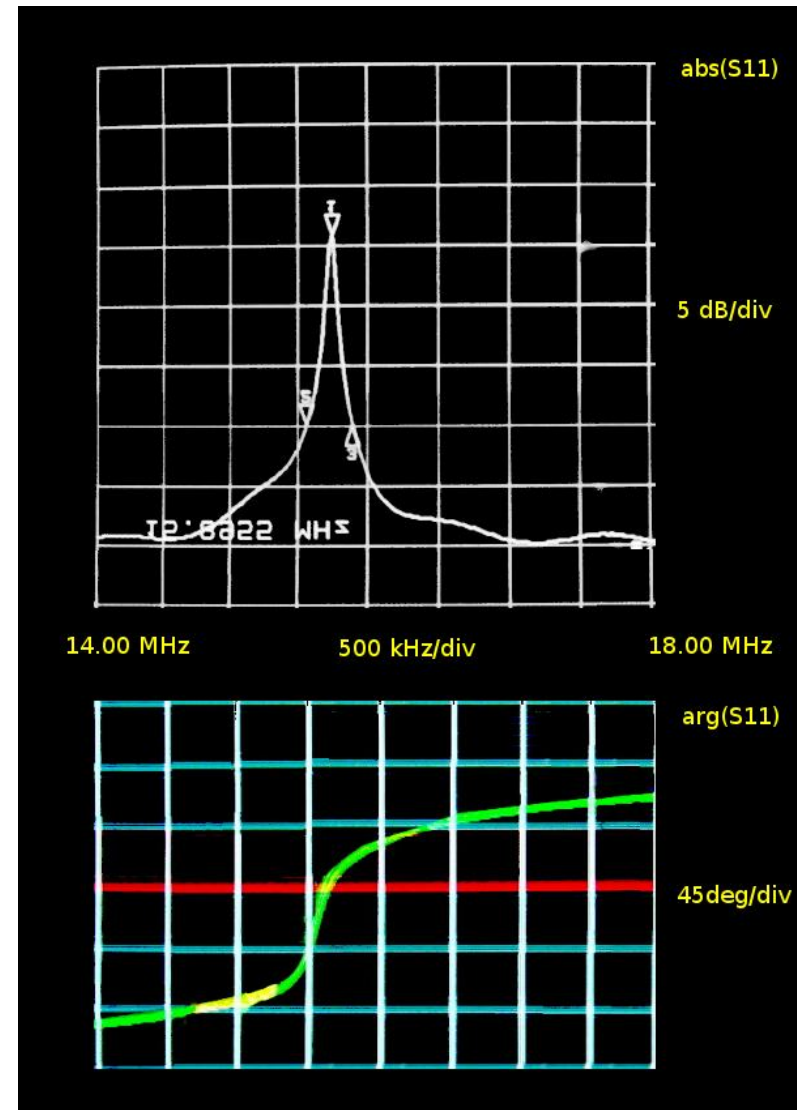
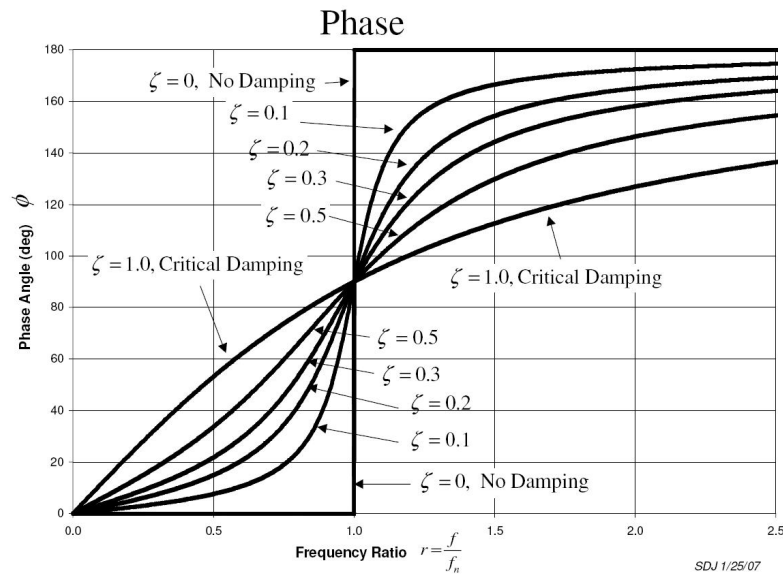
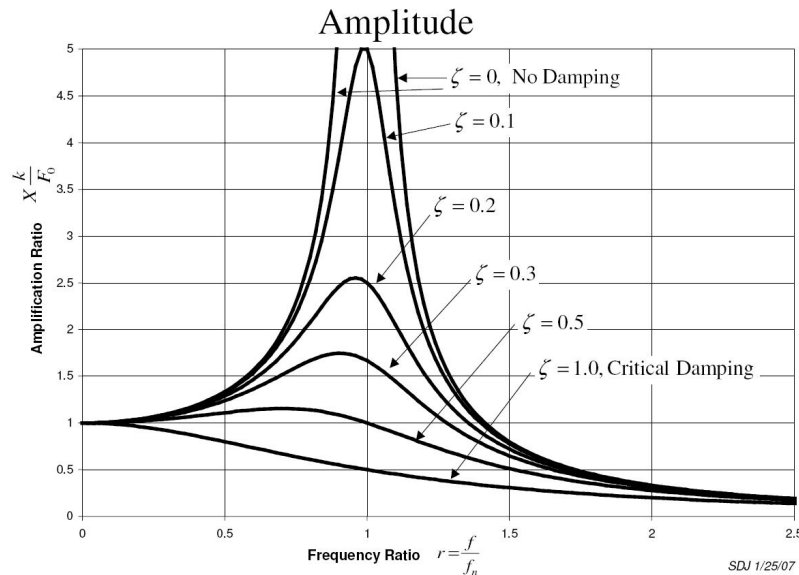
UH-UABC monopole (2008): 8 to 30 MHz, >200 built

- geometric scaling defines frequency

item	length	general	length 4.46 MHz	length 8.25 MHz	length 13.5 MHz	length 16 MHz	length 27 MHz
wavelength	λ		67.26 m	36.36 m	22.22 m	18.75 m	11.11 m
vertical wire	$\lambda/4$		16.8 m	9.09 m	5.55 m	4.69 m	2.78 m
radial wires	$\lambda/4$		16.8 m	9.09 m	5.55 m	4.69 m	2.78 m
pole height	$\lambda/8$		8.4 m	4.55 m	2.78 m	2.35 m	1.29 m
pole diameter	$\lambda/300$		22.4 cm	12 cm	7.5 cm	6.3 cm	3.7 cm



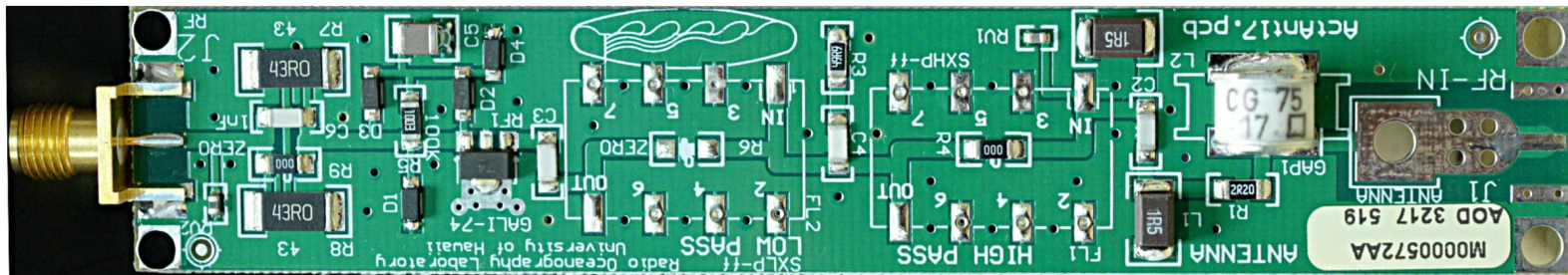
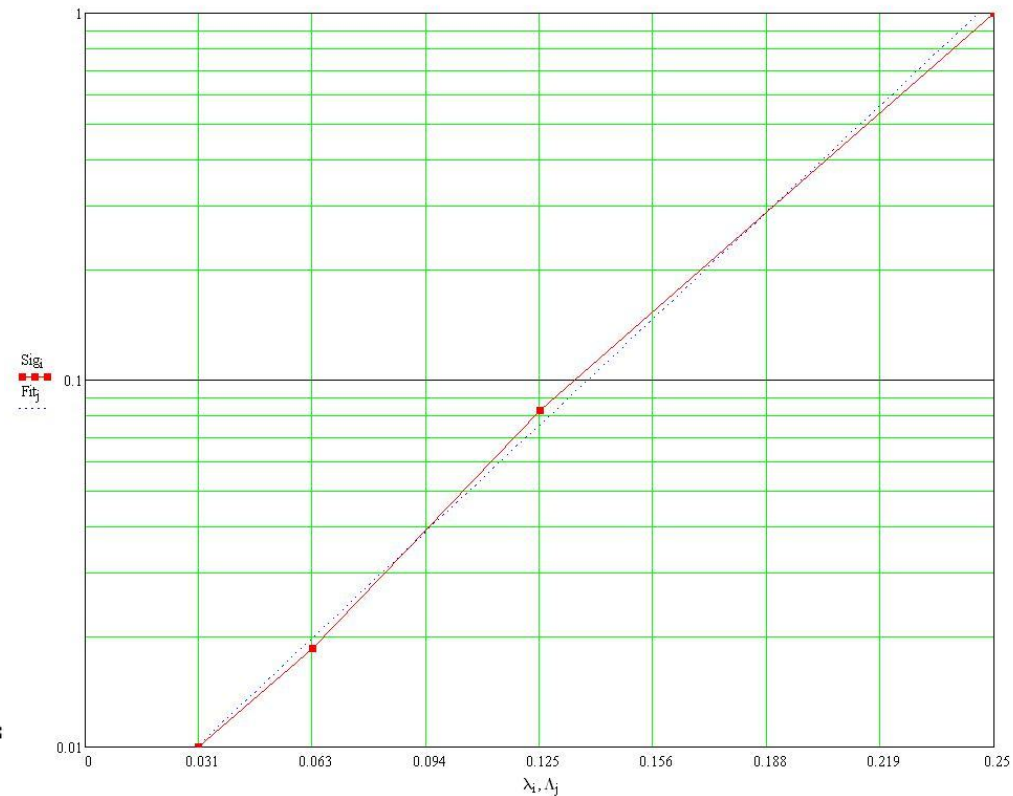
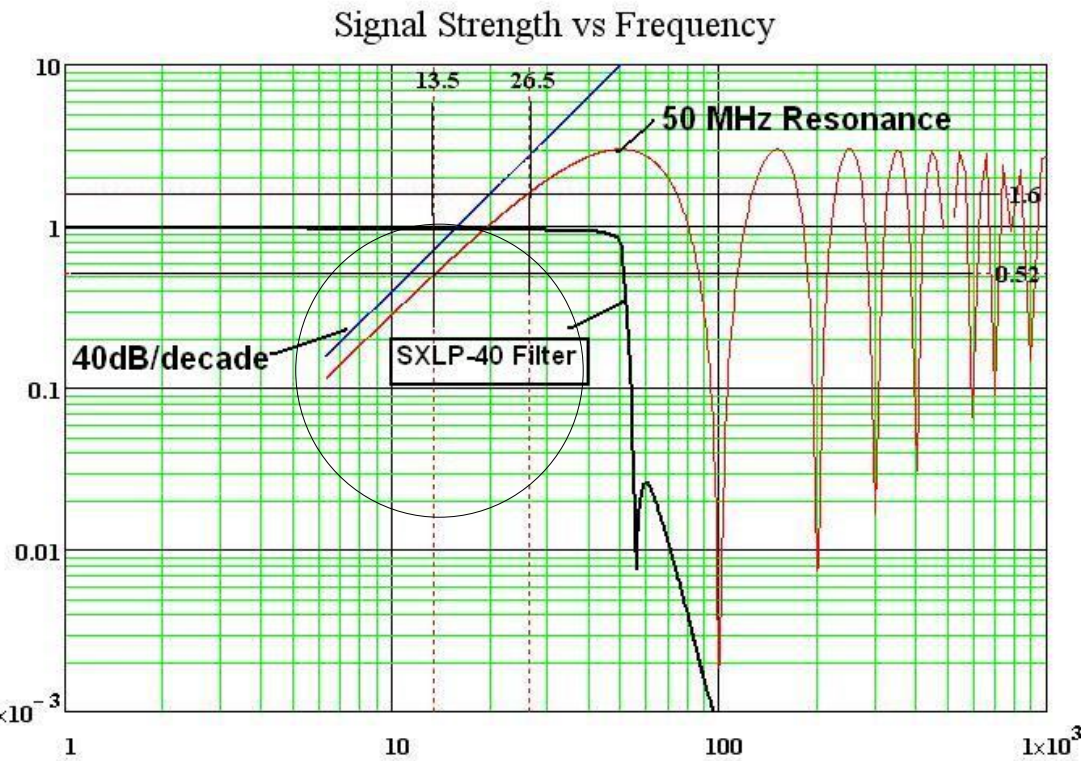
Passive antennas bad for phased-array RX!



Y. Barbin, on U.H. antenna (2002)

- stable tuning to better than 30 kHz difficult
- random phase array errors as chirp passes through resonance point

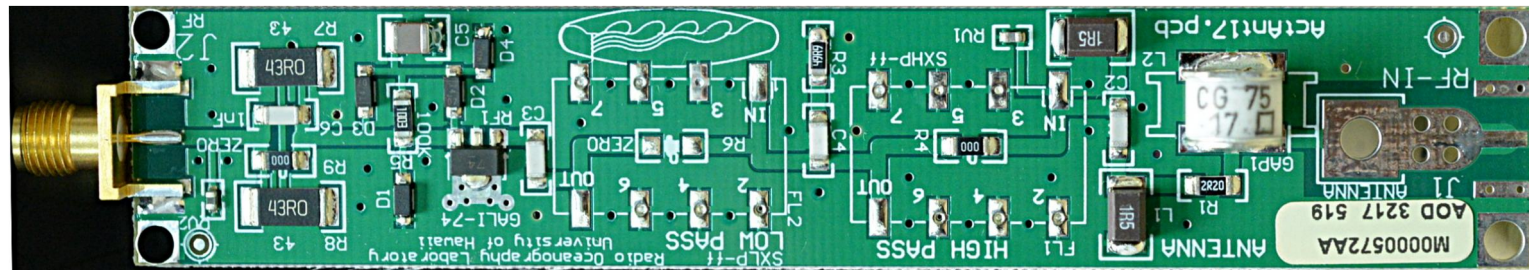
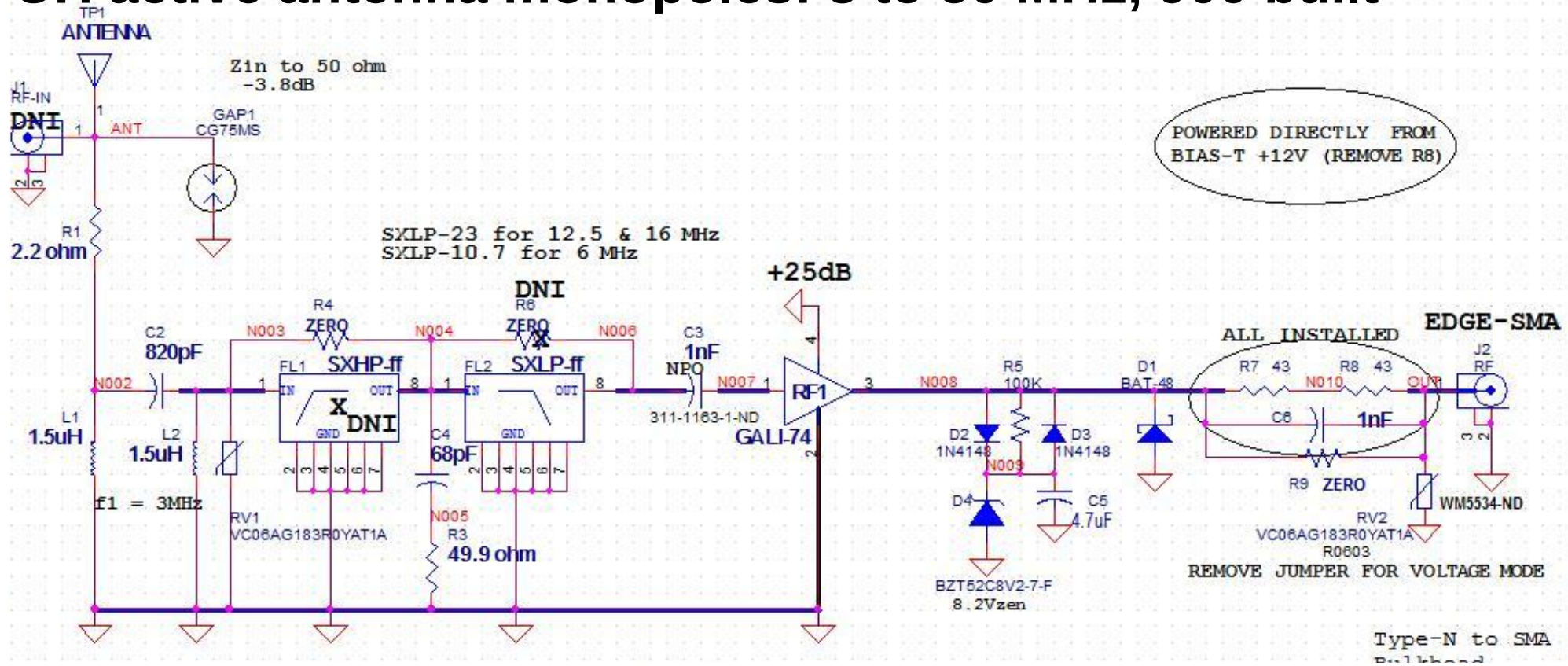
UH active antenna monopoles: 3 to 50 MHz, 900 built



- $\lambda/20$ to $\lambda/8$ wire
- shortened monopole used below resonance point
- low-pass filter at $1.5*f$ (Minicircuits SLXP-40+)
- optional high-pass filter
- 24 dB LNA with 2.7 dB noise figure
- no tuning, no radials



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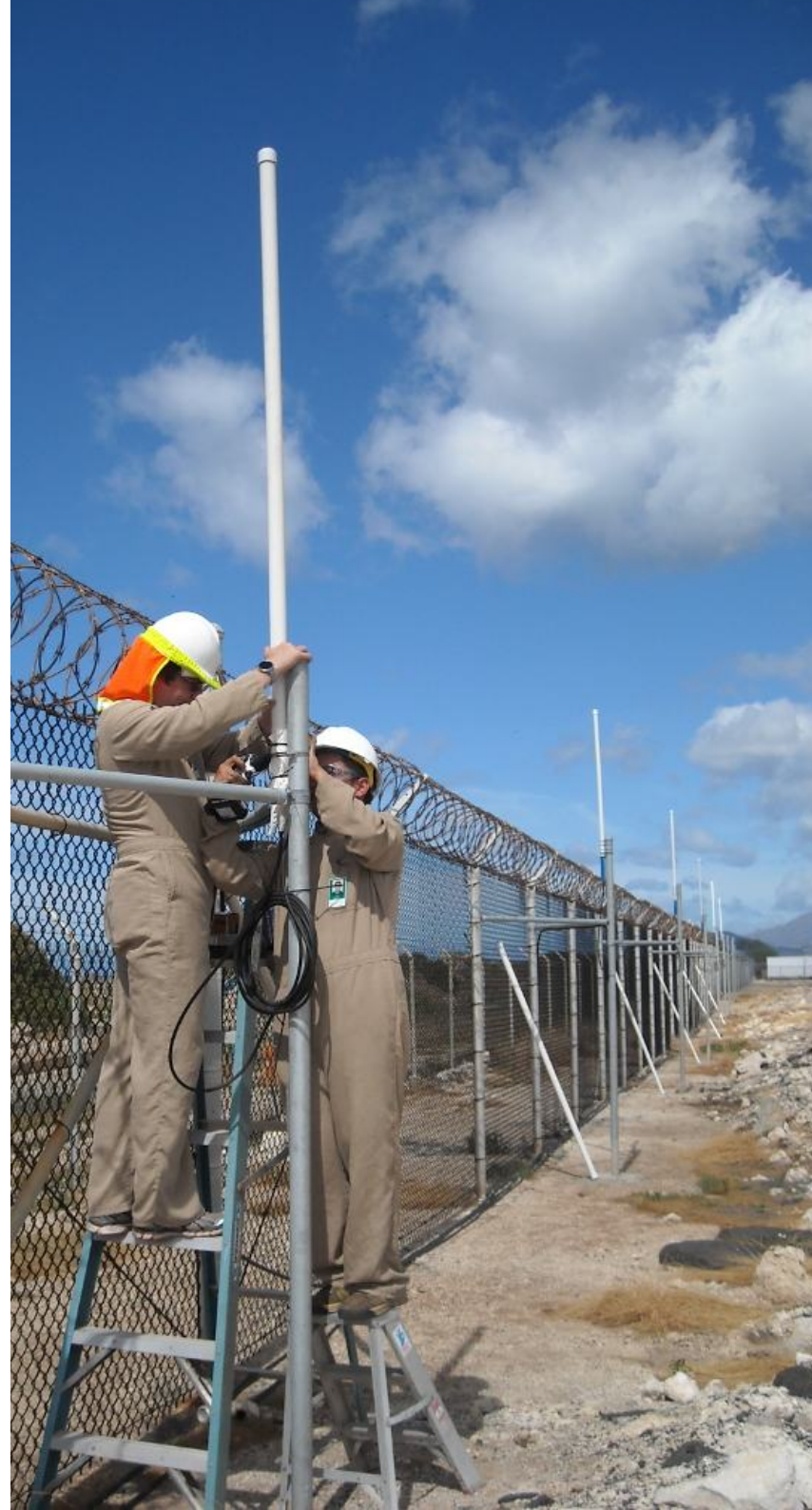
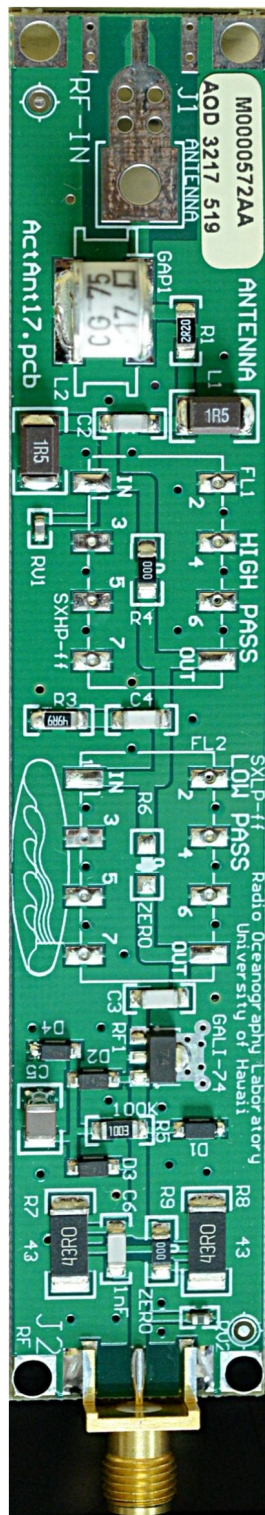


**Active antenna array:
13.5 MHz range 130 km
(Chevron Kapolei)**

$$\lambda = 22.2 \text{ m}$$

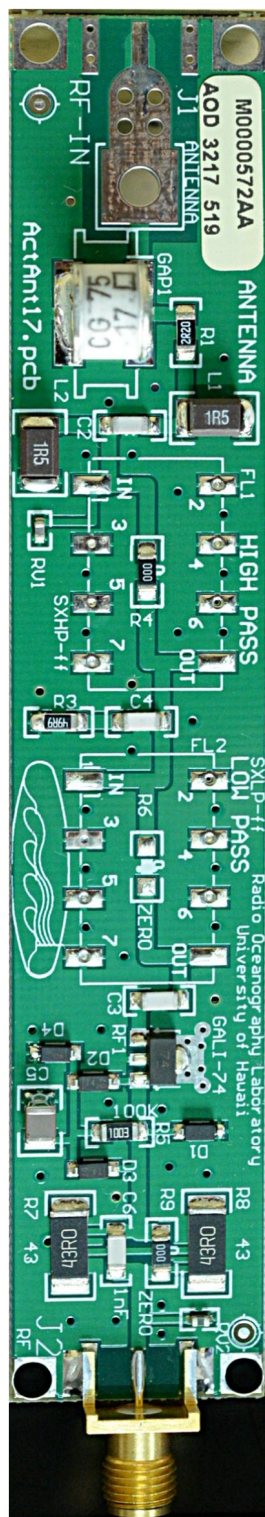
$\lambda/12$ wire strait

$\lambda/12$ PVC mast



**Active antenna array:
16.2 MHz range 80 km
(Martha's Vineyard)**

$\lambda = 18.7 \text{ m}$
 $\lambda/8$ wire coiled
 $\lambda/16$ mast



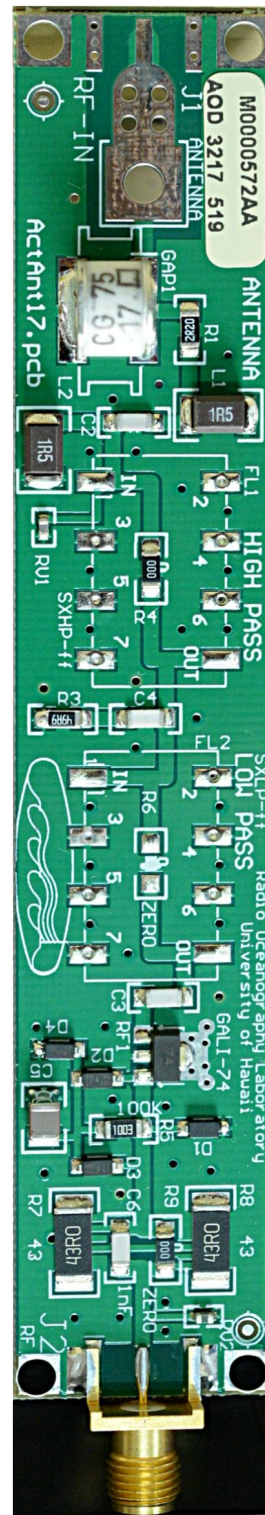
Active antenna for field strength surveying

SOKKIA wood tripod

$\lambda = 18.7 \text{ m}$

$\lambda/8$ wire coiled

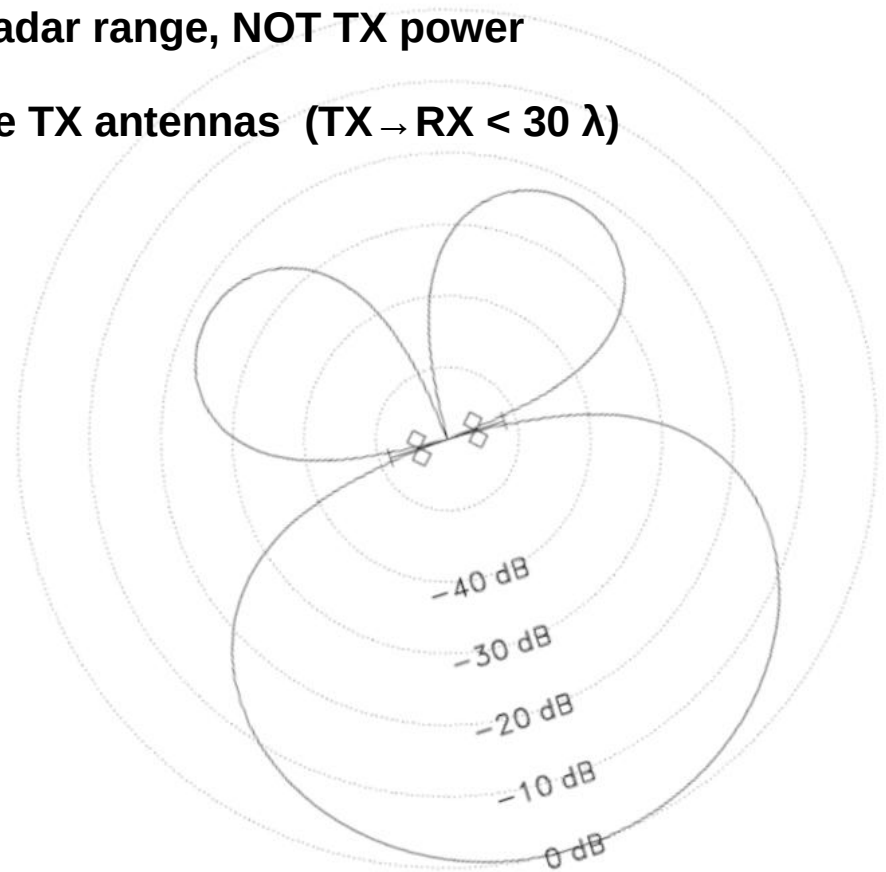
$\lambda/16$ mast



TX beamforming

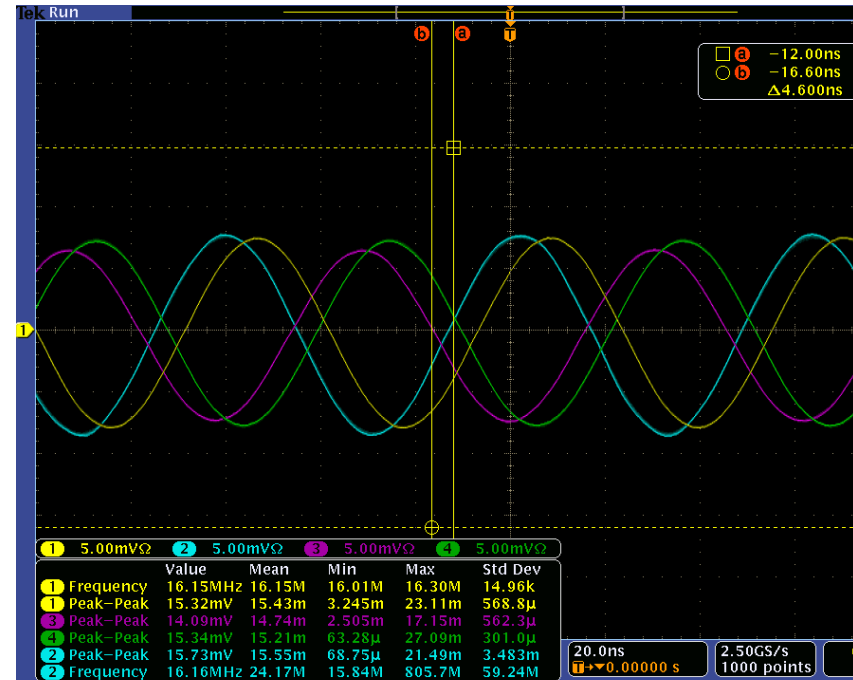
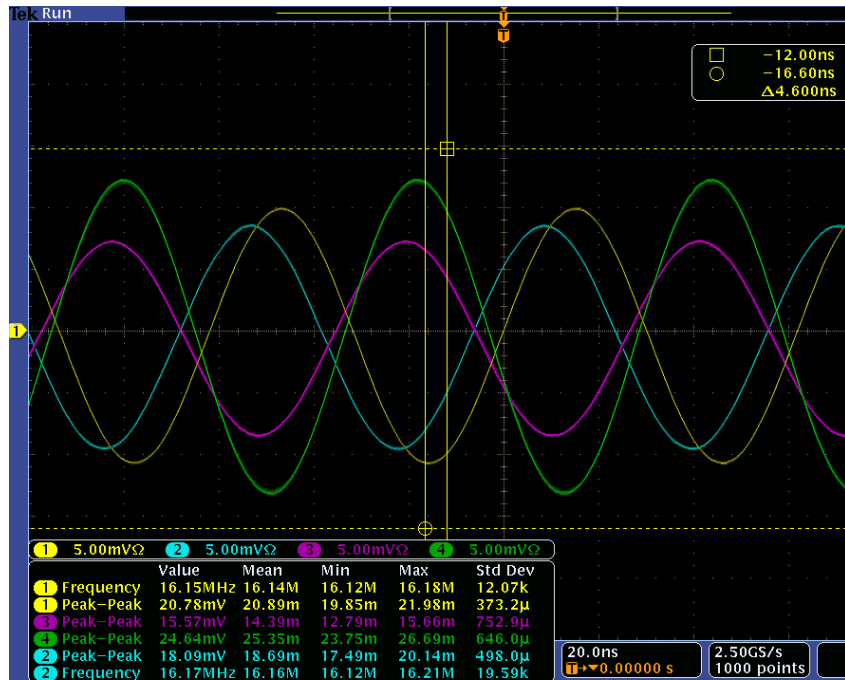
Issue:

- FMCW radars require direct path rejection TX \rightarrow RX
- for given RX sensitivity, direct path governs radar range, NOT TX power
- solution 1: beam-forming on transmit, multiple TX antennas (TX \rightarrow RX $< 30 \lambda$)



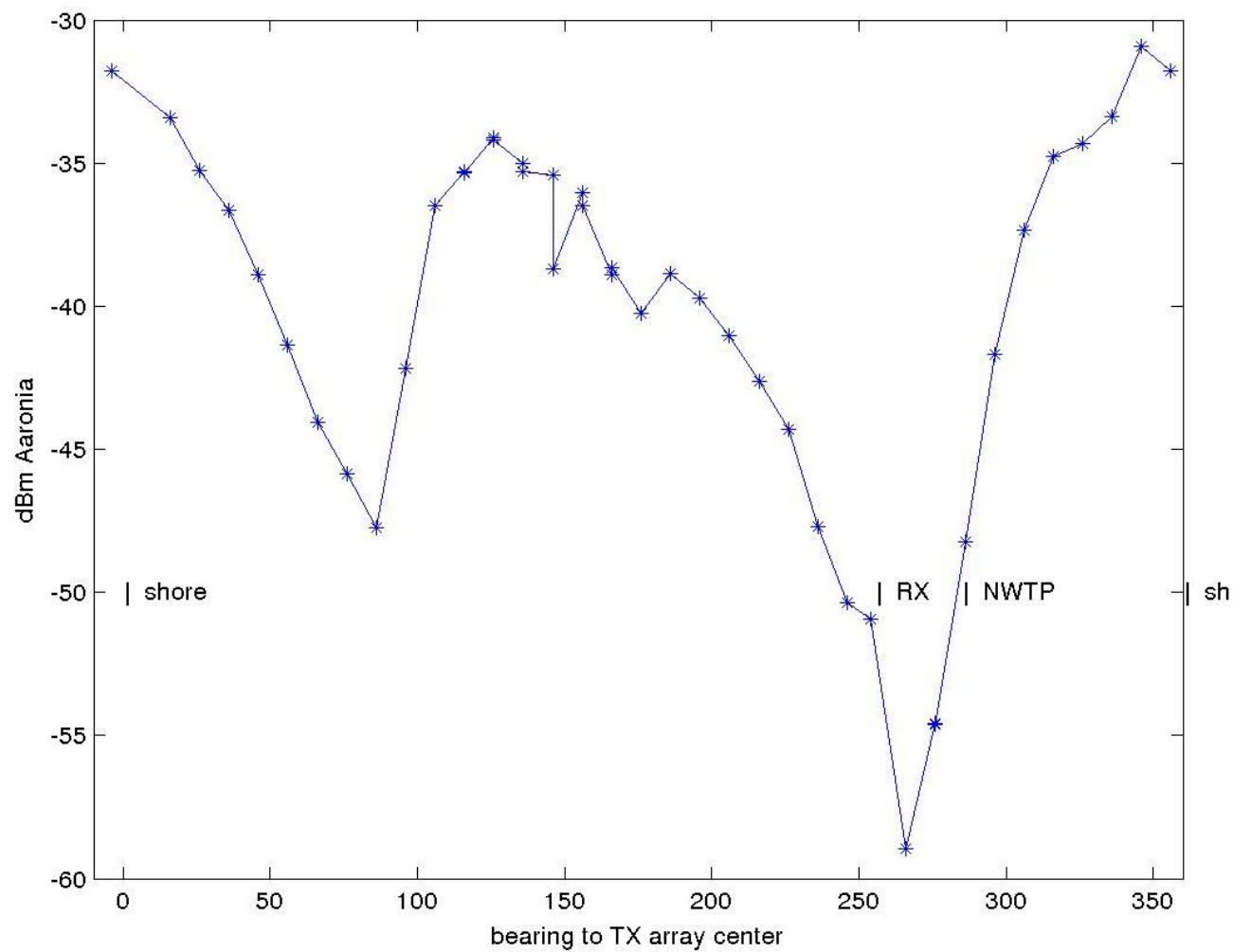
- solution 2: large distance between TX and RX (TX \rightarrow RX $> 40 \lambda$)
(Goro: 900 m @ 16 MHz, 1 TX antenna enough, isotropic transmission)

TX beamforming



- transmit sine wave from passive RX antenna
- 4-channel scope to sample each TX antenna
- adjust amplitude with power attenuators

Mapping TX B-field



Mapping TX B-field

